

Launch vehicle optimization

1. Orbital Mechanics for engineering students

Chapter – 11: Rocket vehicle dynamics

2. Space Flight Dynamics

By William E Wiesel

Chapter 7 – Rocket Performance

Restricted staging in field-free space

No gravity and no aerodynamics

$$\Delta v = I_{sp} g_0 \ln \frac{m_0}{m_f} \quad \frac{m_0}{m_f} = e^{\frac{\Delta v}{I_{sp} g_0}}$$

$$\Delta m = m_0 - m_f;$$

$$\frac{\Delta m}{m_0} = 1 - e^{-\frac{\Delta v}{I_{sp} g_0}}$$

Let gross mass of a launch vehicle $m_0 =$
empty mass $m_E +$
propellant mass $m_p +$
payload mass m_{PL}

Empty mass $m_E =$ mass of structure + mass of fuel tank
and related system + mass of control system

Let us divide the above by m_0

We can write as

$$\pi_E + \pi_p + \pi_{PL} = 1$$

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structural fraction , $\pi_E = m_E / m_0$

Propellant fraction, $\pi_p = m_p / m_0$

payload fraction, $\pi_{PL} = m_{PL} / m_0$

Alternately we can define

$$\text{Payload ratio } \lambda = \frac{m_{PL}}{m_E + m_p} = \frac{m_{PL}}{m_0 - m_{PL}}$$

Structural ratio $\varepsilon = \frac{m_E}{m_E + m_p} = \frac{m_E}{m_0 - m_{PL}}$

Mass ratio $n = \frac{m_0}{m_f}$

Assuming all the propellant is consumed $n = \frac{m_E + m_p + m_{PL}}{m_E + m_{PL}}$

λ , ε and n are not independent

From $\varepsilon = \frac{m_E}{m_E + m_p}$ we can write as

$$m_E = \frac{\varepsilon}{1 - \varepsilon} m_p$$

From $\lambda = \frac{m_{PL}}{m_E + m_p}$ we can write as

$$\begin{aligned} m_{PL} &= \lambda(m_E + m_p) = \lambda \left(\frac{\varepsilon}{1 - \varepsilon} m_p + m_p \right) \\ &= \frac{\lambda}{1 - \varepsilon} m_p \end{aligned}$$

Substituting $m_E = \frac{\varepsilon}{1 - \varepsilon} m_p$ and

$m_{PL} = \frac{\lambda}{1 - \varepsilon} m_p$ in

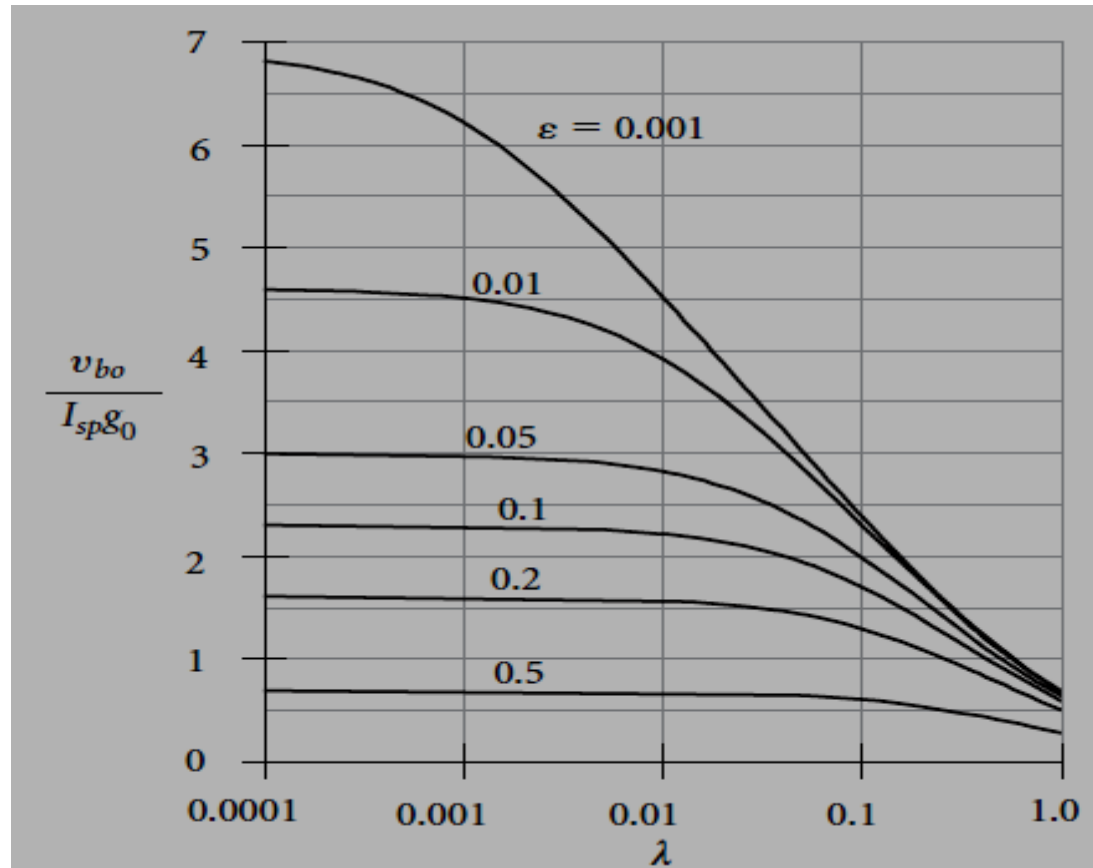
$$n = \frac{m_E + m_p + m_{PL}}{m_E + m_{PL}}$$

We get $n = \frac{1 + \lambda}{\varepsilon + \lambda}$

Given any two of the ratios λ , ε and n , we can obtain the third

Velocity at burn out is

$$v_{bo} = I_{sp}g_0 \ln n = I_{sp}g_0 \ln \frac{1 + \lambda}{\varepsilon + \lambda}$$

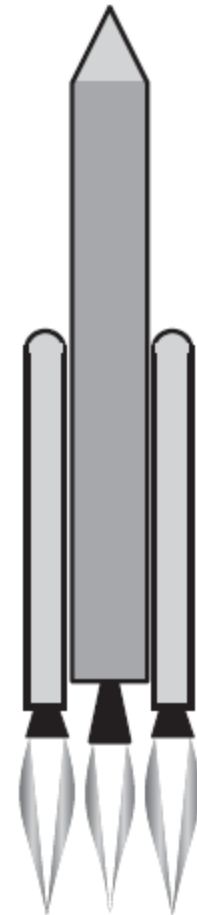
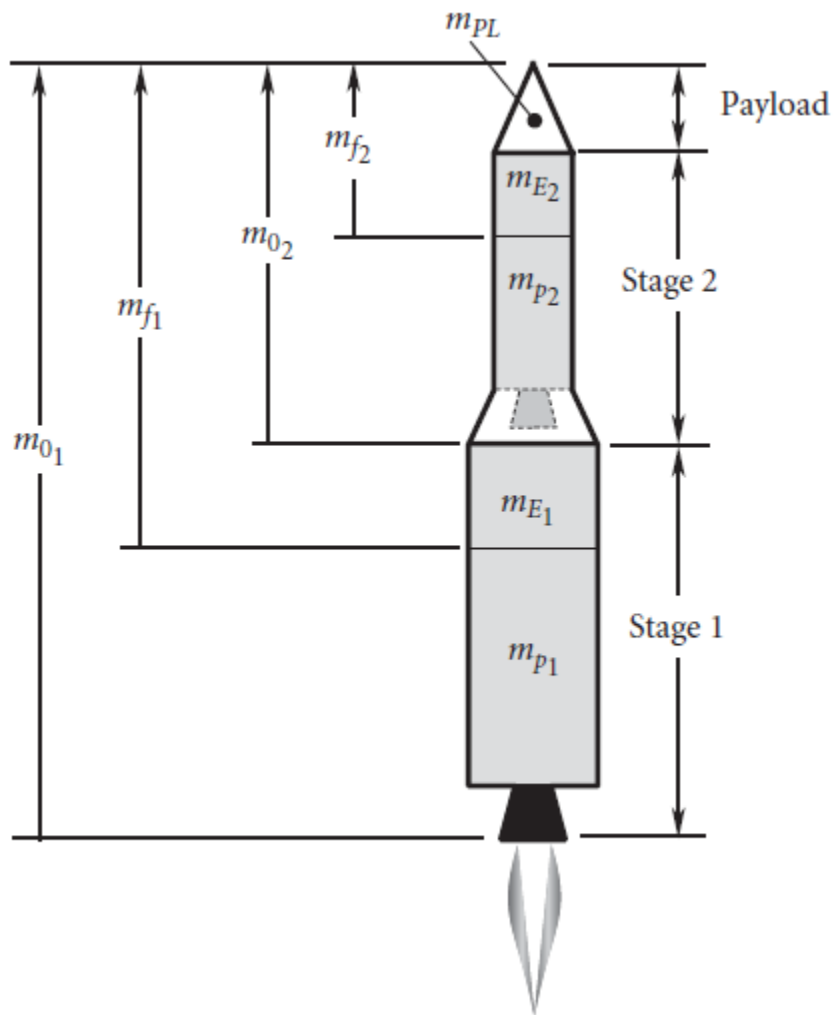


For a given empty mass, the greatest possible Δv occurs when the payload is zero.

To maximize the amount of payload while keeping the structural weight to a minimum.

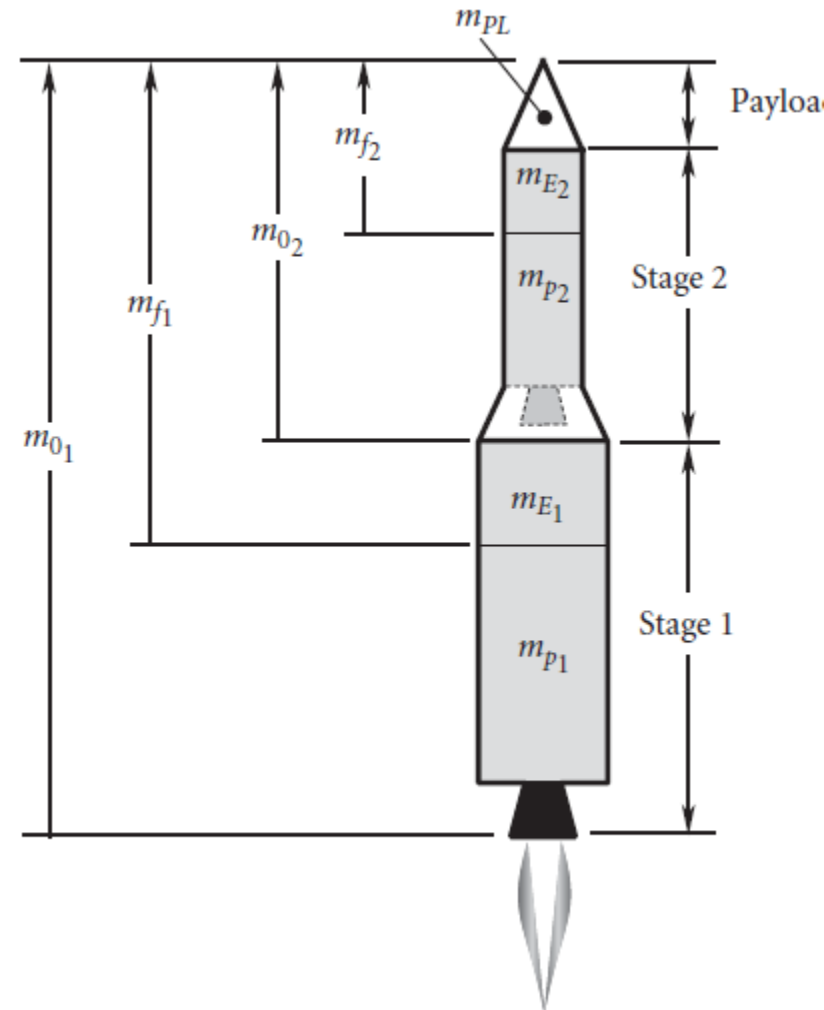
Mass of load-bearing structure, rocket motors, pumps, piping, etc., cannot be made arbitrarily small.

Current materials technology places a lower limit on ϵ of about 0.1.



Performance of multistage rocket

Restricted staging - all stages are similar
Each stage has the
same specific impulse I_{sp}
same structural ratio ϵ
same payload ratio λ .
Hence mass ratios n are identical



Final burnout speed v_{bo} for a given payload mass m_{PL}

Overall payload fraction $\pi_{PL} = \frac{m_{PL}}{m_0}$

m_0 is the total mass of the tandem-stacked vehicle.

For a single-stage vehicle, the payload ratio is

$$\lambda = \frac{m_{PL}}{m_0 - m_{PL}} = \frac{1}{\frac{m_0}{m_{PL}} - 1} = \frac{\pi_{PL}}{1 - \pi_{PL}}$$

$$\lambda = \frac{\pi_{PL}}{1 - \pi_{PL}}$$

From the equation $n = \frac{1 + \lambda}{\varepsilon + \lambda}$

The mass ratio is $n = \frac{1}{\pi_{PL}(1 - \varepsilon) + \varepsilon}$

$$v_{bo} = I_{sp}g_0 \ln n = I_{sp}g_0 \ln \frac{1 + \lambda}{\varepsilon + \lambda}$$

$$v_{bo} = I_{sp}g_0 \ln \frac{1}{\pi_{PL}(1 - \varepsilon) + \varepsilon}$$

For a single-stage vehicle burnout speed v_{bo} for a given payload mass m_{PL}

$$v_{bo} = I_{sp} g_0 \ln \frac{1}{\pi_{PL}(1 - \varepsilon) + \varepsilon}$$

In the book “ Space Flight Dynamics” by William E Wiesel
The above expression is given as

$$v_{bo} = -v_e \ln[\varepsilon + (1 - \varepsilon) \pi]$$

Let m_0 be the total mass of the two-stage rocket

$$m_0 = m_{01}$$

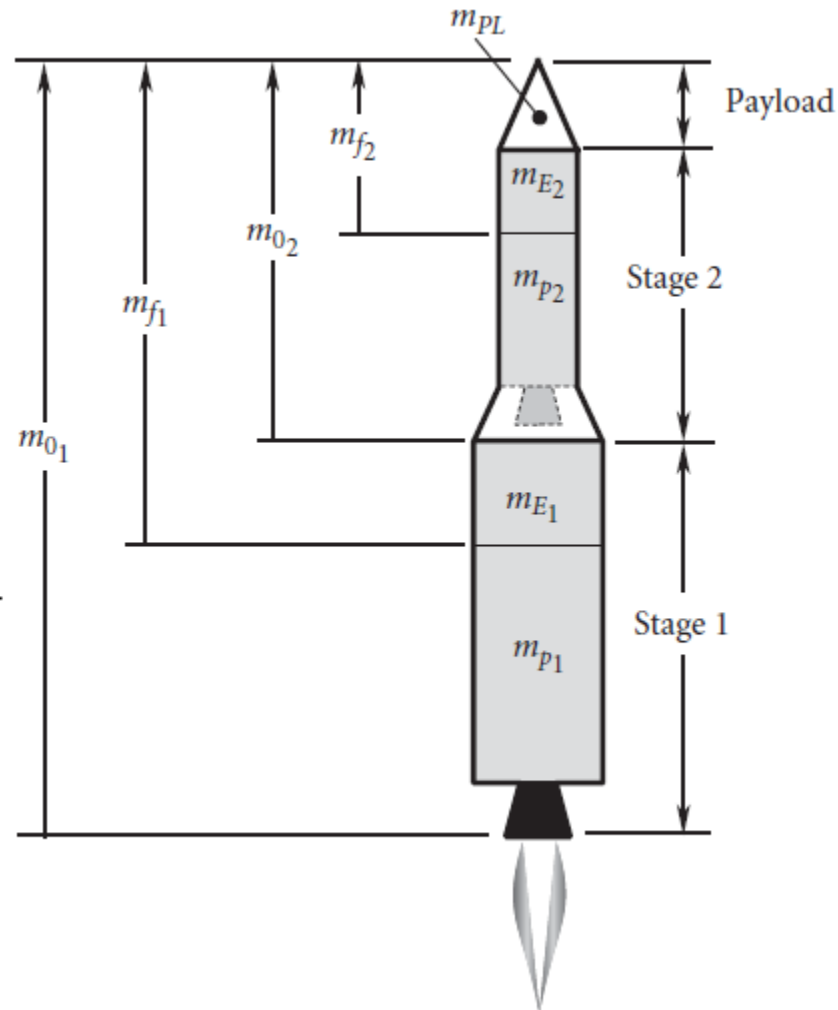
payload of stage 1 is the entire mass m_{02} of stage 2

stage 1 payload ratio is

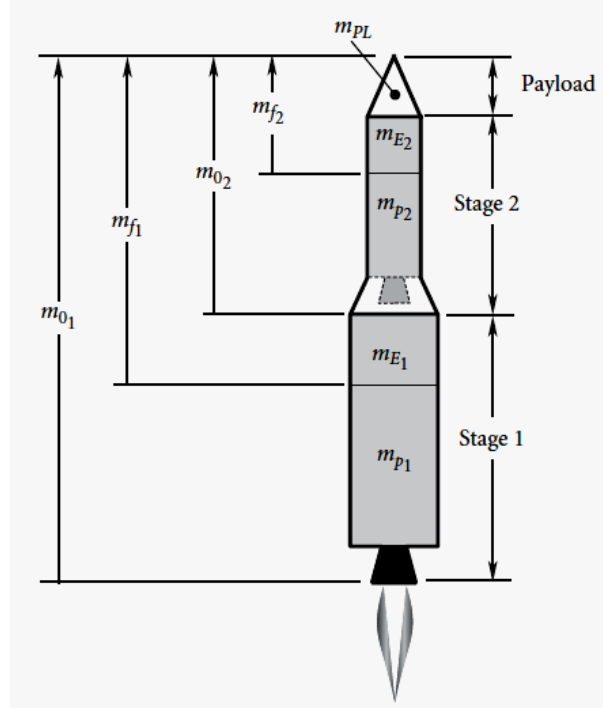
$$\lambda_1 = \frac{m_{02}}{m_{01} - m_{02}} = \frac{m_{02}}{m_0 - m_{02}}$$

payload ratio of stage 2 is

$$\lambda_2 = \frac{m_{PL}}{m_{02} - m_{PL}}$$



And continues.....



$$m_{E1} = \frac{\left(1 - \pi_{PL}^{\frac{1}{2}}\right) \varepsilon}{\pi_{PL}} m_{PL}$$

$$m_{E2} = \frac{\left(1 - \pi_{PL}^{\frac{1}{2}}\right) \varepsilon}{\pi_{PL}^{\frac{1}{2}}} m_{PL}$$

$$m_{P1} = \frac{\left(1 - \pi_{PL}^{\frac{1}{2}}\right) (1 - \varepsilon)}{\pi_{PL}} m_{PL}$$

$$m_{P2} = \frac{\left(1 - \pi_{PL}^{\frac{1}{2}}\right) (1 - \varepsilon)}{\pi_{PL}^{\frac{1}{2}}} m_{PL}$$

For a multi stage rockets

$$v_{bo} = \sum_{k=1}^n -v_{ek} \ln [\epsilon_k + (1 - \epsilon_k) \pi_k]$$

Calculate the v_e ($g_0 * I_{sp}$), ϵ_k , for π_k each stage
Sequentially and sum up

Example 11.2 – Page No: 566

The following data is given

$$m_{PL} = 10\,000 \text{ kg}$$

$$\pi_{PL} = 0.05$$

$$\varepsilon = 0.15 \tag{a}$$

$$I_{sp} = 350 \text{ s}$$

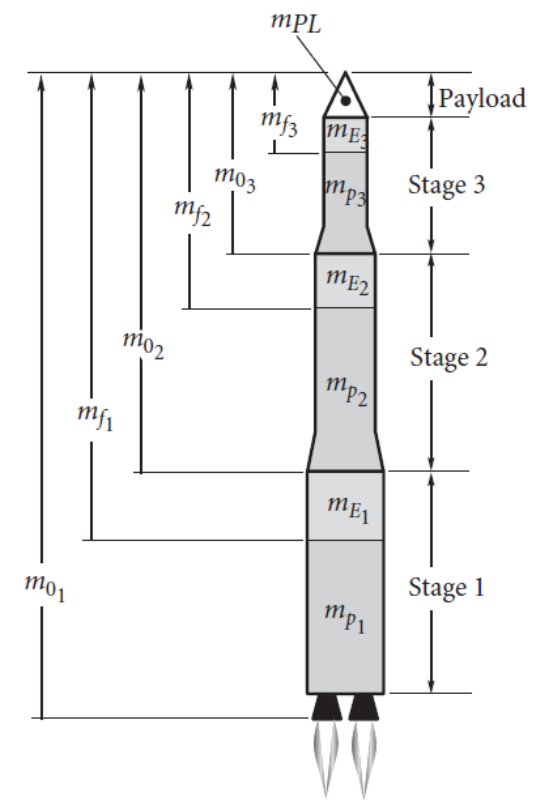
$$g_0 = 0.00981 \text{ km/s}^2$$

Calculate the payload velocity v_{bo} at burnout, the empty mass of the launch vehicle and the propellant mass for (a) a single stage and (b) a restricted, two-stage vehicle.

$$m_{p_1} = \frac{\left(1 - \pi_{PL}^{\frac{1}{3}}\right) (1 - \varepsilon)}{\pi_{PL}} m_{PL}$$

$$m_{p_2} = \frac{\left(1 - \pi_{PL}^{\frac{1}{3}}\right) (1 - \varepsilon)}{\pi_{PL}^{\frac{2}{3}}} m_{PL}$$

$$m_{p_3} = \frac{\left(1 - \pi_{PL}^{\frac{1}{3}}\right) (1 - \varepsilon)}{\pi_{PL}^{\frac{1}{3}}} m_{PL}$$



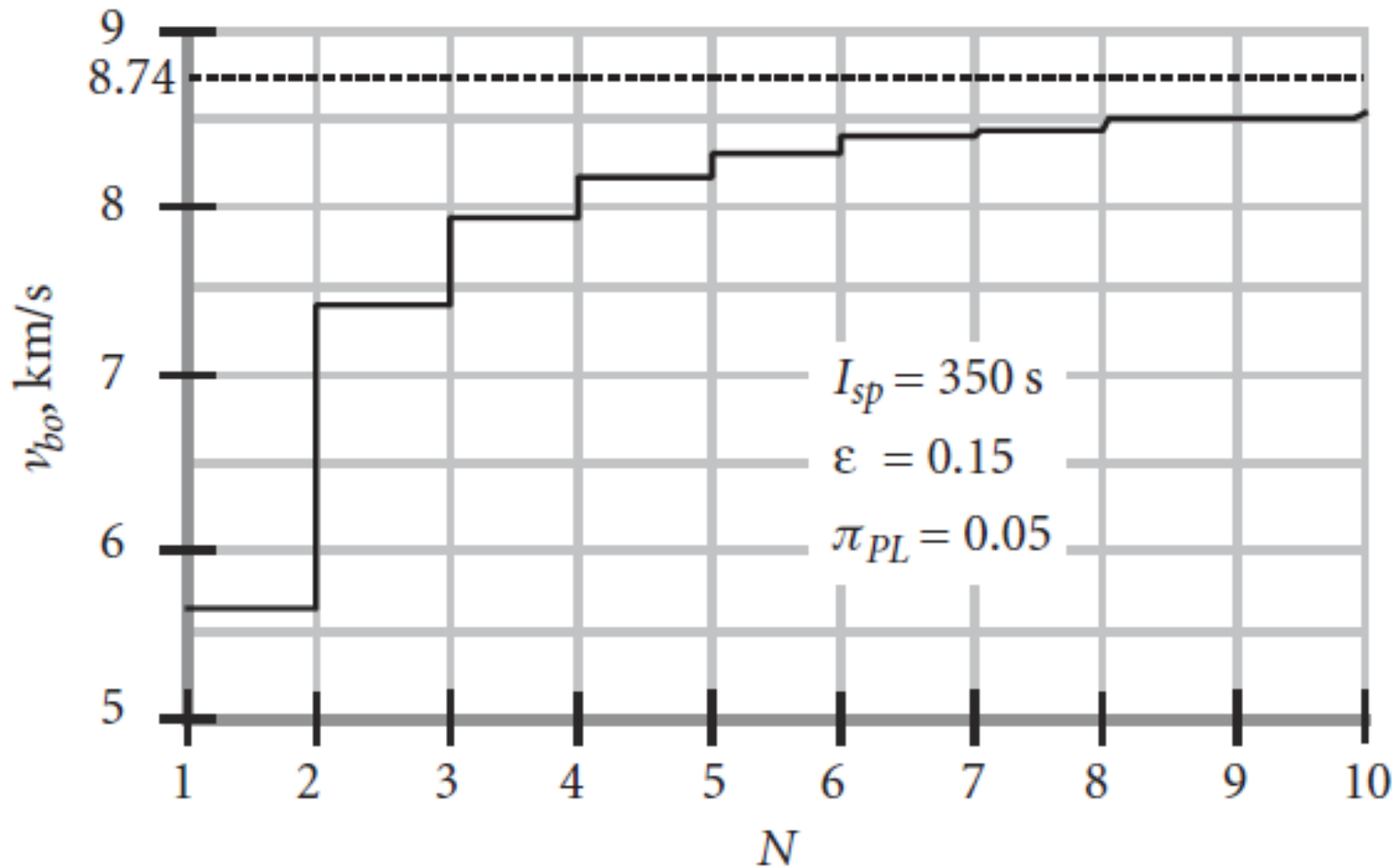
$$m_{E_1} = \frac{\left(1 - \pi_{PL}^{\frac{1}{3}}\right) \varepsilon}{\pi_{PL}} m_{PL}$$

$$m_{E_2} = \frac{\left(1 - \pi_{PL}^{\frac{1}{3}}\right) \varepsilon}{\pi_{PL}^{\frac{2}{3}}} m_{PL}$$

$$m_{E_3} = \frac{\left(1 - \pi_{PL}^{\frac{1}{3}}\right) \varepsilon}{\pi_{PL}^{\frac{1}{3}}} m_{PL}$$

Example 11.3

Repeat Example 11.2 for the restricted three-stage launch vehicle.



Zeroth stage – combined I stage
And strapped on boosters

Boosters burn out fast and separated

Balance propellant of the core
I stage burns

How to calculate????????

Assignment!!

